

OVERVIEW OF DESIGNING THE LOAD MATCHING NETWORK FOR A POWER AMPLIFIER BY USING THE CIL WIZARD PROVIDED IN THE AMPSA ADW

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The ADW is setup to design single-ended amplifiers. Note that Doherty amplifiers, balanced amplifiers, push-pull amplifiers, amplifiers with symmetrical combination networks and even some load modulated balanced amplifiers can all be converted to equivalent single-ended stages.

The Ampsa ADW CIL wizard can be used to set up a large variety of matching problems for an amplifier stage. Different classes of operation can be targeted. These include continuous modes of operation.

In this presentation, the CIL wizard will be used to setup the specifications for the load matching network of a 1.0 – 3.9 GHz 10W amplifier. Solutions to the defined problem will also be synthesized by using the impedance-matching wizard provided in the ADW.

The Macom CGH40010F GaN transistor will be used in this example. An ADW model was fitted to the transistor biased at 28V 200mA (Class-AB operation). Class-B operation will be targeted in this presentation, but the same design flow can be used for other classes of operation.



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Scale Factor = 0.529x (40.10E3um x 25.35E3um)



The circuit shown will be used as a starting point for the design. The input matching network is from a previous design, but the design flow is still valid without an input matching network in place. (Stabilizing the transistor, at least inside the passband is, however, advisable.) The input network can be optimised when the load network is in place.

Note that the schematic or the artwork or the text description of the circuit can be viewed. Use the commands provided on the quick access toolbar (QAT) to switch between views.



The ADW synthesis wizards must be launched with a schematic view active. The insertion point for the matching network required must be selected before launching the wizard.

Note that an element in the schematic is selected by left-clicking one of the labels associated with the schematic element. In an artwork view, the artwork element to be selected is left-clicked.



The CIL wizard was launched by selecting the Schematic | Wizards | CIL ribbon command. The schematic will be split as shown by the command.

The matching network to be designed with the CIL wizard can be the load network for the output stage or any driver stage in the amplifier. A multistage power amplifier is designed by starting with the load network.



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CIL/CIR Impedance-Matching Wizard			×	
Description				
Mare control over the energiestions of a s	natching naturals is possible when the CII			
CIR commands are used. The actual spec	cifications are then decided in the ADW Power			
or Circle Module. The position of the netw the parameters required by the Power/Circ	ork and the passband are set at this point, and cle Module are calculated.			
The CIL command is used when the desig	n proceeds from the load towards the source			
and vice versa for the CIR command. The	e output power, operating power gain or the			
command is used to control the noise figur	re or the available power gain, and can also be			
7 used to control the transducer power gain	•			
			0MA 42.368/Ω 3.9921°	49.23Ω 9.9882° (E=3.9GHz: GT)
< Input side 🖛	- Output side			
Z ₅	ZL			
		< Back Next > Cancel H	Help	
Ready				i:

The first page of the CIL wizard is displayed here.



CIL/CIR Impedance-Matching Wizard - Contour Option

When the CIL command is used, the transducer power gain, the operating power gain or the output power of the stage selected can be controlled directly. The transducer power gain, the available power gain or the noise figure can be controlled directly when the CIR command is used.

Performance to be Controlled

Operating power gain (Conjugate match required on the input side)

O Transducer power gain (Input matching network in place or not required)

Output power

The operating power gain or the transducer power gain or the output power of the stage designed can be controlled by the CIL wizard. The option to control the power was selected here.

< <u>B</u> ack <u>N</u> ext > Cancel Help

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CIL/CIR Wizard - Power Module Options

When the power performance is controlled, the output power or the effective output power (Pout-Pin) can be specified. The gain calculated on the contours can also be specified to be the transducer power gain, or the available/operating power gain of the stage/section of interest (The transducer power gain option should be used when the input matching network is already in place). The option to specify the power termination or to specify the contours to be generated is also provided.

Power Option

Control the output power (Pout)

Control the effective output power (Pout-Pin)

Gain Control Option

Control Gw (Conjugate match required on the input side)
 Control GT (Input matching network, if any, in place)

Specifications Option

O Specify the external load

O Specify the intrinsic load

Specify power contours

Impedance-Matching Option

Set ZLi as synthesis target

The output power or the effective output power can be controlled. Use the effective output power when the transistor gain is low or when a matching network for an oscillator is designed.

When an input matching network is already in place, the gain to be controlled is the transducer power gain. This option was selected here.

The power contours option was selected here. The alternatives are to control the intrinsic or external load terminations directly.

Note the option to use the intrinsic load terminations as synthesis targets. When this option is not selected, the input terminations presented by the matching network at the insertion point are used as targets.

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Cancel

Help

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Next >

CIL/CIR Wizard - Power Specifications

The maximum unclipped power (dBm) required at each frequency must be specified below. The power specified must be less or equal to the maximum power. Two additional contours can also be displayed graphically. Use the error function weights and zero error points commands to define the error function used to decide the default optimum point on each power contour targeted.

Power (dBm) Required at Each Frequency

F(GHz)	PmuMax (P)	PmuRq(dBm)	PmuC2 (dBm)	PmuC3 (dBm)	Eff@PeakP	Eff@Tgt	
1.0000	40.578	40.578	39.578	38.578	61.760	61.760	
1.1000	40.578	40.578	39.578	38.578	61.765	61.765	
1.2000	40.578	40.578	39.578	38.578	61.767	61.767	
1.3000	40.578	40.578	39.578	38.578	61.761	61.761	
1.4000	40.578	40.578	39.578	38.578	61.767	61.767	
1.5000	40.579	40.579	39.579	38.579	61.772	61.772	
1.6000	40.579	40.579	39.579	38.579	61.774	61.774	
1.7000	40.579	40.579	39.579	38.579	61.777	61.777	
1.8000	40.579	40.579	39.579	38.579	61.780	61.780	
1.9000	40.580	40.580	39.580	38.580	61.785	61.785	
2.0000	40.580	40.580	39.580	38.580	61.787	61.787	
2.1000	40.580	40.580	39.580	38.580	61.792	61.792	
2.2000	40.570	40.580	39.580	38.580	61.794	61.794	
ErrFnc <u>Z</u> ero	Points	Edit <u>A</u> bsolute	<u>S</u> ummary	Table			
		PoAtPeakEff					
aximum-Effici	iency (ME) amd	Minimum Accept	able Efficiency (MAE) Lines		Classes B, F and iF Efficiency (FFLL)	
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Show Show	+X MAF Lines	[5; 51] <	10>	Enciency	/ (/₀):	Enciency Fitting 0.000 <0.0>	

The power levels of interest must be specified on this page. Constant power contours can also be generated at two additional power levels at each frequency.

The error function used to select the optimum point on each contour is set by using the Error Function Weights and Zero Error Points commands.

Edit Relative or Edit Absolute are used to set the contour power levels.

The efficiency associated with the peak power points and the maximum efficiency associated with the contours targeted are also listed in the table.

Note that the minimum acceptable efficiency must be specified for the efficiency lines to be displayed. (With the exception of a Class-A stage, the efficiency will vary on the circumference of each power contour.)

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The option to use only the efficiency to decide the optimum point on each constant power contour targeted has been selected (Error Function Weights command).

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CIL/CIR Wizard - Power Specifications

The maximum unclipped power (dBm) required at each frequency must be specified below. The power specified must be less or equal to the maximum power. Two additional contours can also be displayed graphically. Use the error function weights and zero error points commands to define the error function used to decide the default optimum point on each power contour targeted.

Power (dBm) Required at Each Frequency



The Edit Relative command has been selected to set the power levels for the contours to be generated. The power level targeted is 0.6 dBm below the peak power.

X

CIL/CIR Wizard - Power Specifications

The maximum unclipped power (dBm) required at each frequency must be specified below. The power specified must be less or equal to the maximum power. Two additional contours can also be displayed graphically. Use the error function weights and zero error points commands to define the error function used to decide the default optimum point on each power contour targeted.

Power (dBm) Required at Each Frequency

F(GHz)	PmuMax(P)	PmuRq(dBm)	PmuC2 (dBm)	PmuC3 (dBm)	Eff@PeakP	Eff@Tgt	
1.0000	40.578	39.978	39.778	39.578	61.760	70.376	
1.1000	40.578	39.978	39.778	39.578	61.765	70.378	
1.2000	40.578	39.978	39.778	39.578	61.767	70.376	
1.3000	40.578	39.978	39.778	39.578	61.761	70.365	
1.4000	40.578	39.978	39.778	39.578	61.767	70.364	
1.5000	40.579	39.979	39.779	39.579	61.772	70.366	
1.6000	40.579	39.979	39.779	39.579	61.774	70.363	
1.7000	40.579	39.979	39.779	39.579	61.777	70.358	
1.8000	40.579	39.979	39.779	39.579	61.780	70.355	
1.9000	40.580	39,980	39.780	39.580	61.785	70.354	
2.0000	40.580	39.980	39.780	39.580	61.787	70.348	
2.1000	40.580	39,980	39.780	39.580	61.792	70.343	
2.2000	40.570	39.970	39.770	39.570	61.794	70.338	
ErrFnc Ve	Points	Edit <u>A</u> bsolute	List Mor	Table	play Contours		
		PoAtPeakEff					
aximum-Effici	iency (ME) amd	Minimum Accept	able Efficiency (MAE) Lines		Classes B, F and iF Efficiency (F	FLL)
Show Show	ME Lines +X MAE Lines	Number of I [5; 51] <	ME Line Points: (15>	Minimum Ac Efficienc	ceptable y (%):	Efficiency Fitting	<0.0>
Show -		15		60	<62.5>	[0.0; 0.1]	-

The power listed here is the maximum unclipped output power (P_{mu}).

Efficiencies (drain efficiency) above 60% are targeted.

The List More command can be used to list the peak efficiency obtainable at different power levels.

The Display Contours command can be used to display the constant power contours and the maximum efficiency lines.

Help

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The constant power contours targeted are shown here with the maximum efficiency lines.

The intrinsic load impedance is purely resistive at the maximum efficiency point on a power contour. This point is located on the voltage clipping side of the power contour.

Note the anti-clockwise rotation of the maximum efficiency lines with increasing frequency (green to magenta). Also note the area in which all the constant power contours intersect and the area in which the maximum efficiency lines intersect.



Optimum Power Terminations



The constant power contours and the efficiency lines at 1.0 GHz and 3.9 GHz are displayed here.

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Three efficiency lines are shown with the power contours at each frequency. The two lines away from the maximum efficiency line are constant efficiency lines.

Efficiencies above the targeted level can only be obtained on the contour sections defined by the two constant efficiency lines.



CIL/CIR Wizard - Potential Performance on the Selected Contours

Area inside circle

Stage Output Power Targeted: 39.98 dBm

Angle (°)	RL (Ω)	XL (Ω)	GT (dB)	Tun	VSWRload	VSWRin	VSWRa	Eff (%)	SSF	LSF
215.317	19.1918	-j1.917	16.109	0.087	2.609	5.425	2.334	54.986	1.217	1.593
227.731	19.3623	-j2.311	16.102	0.087	2.588	5.400	2.343	54.986	1.217	1.584
240.145	19.5666	-j2.772	16.095	0.088	2.564	5.370	2.353	54.997	1.217	1.574
252.559	19.8341	-j3.377	16.084	0.088	2.534	5.332	2.367	55.001	1.217	1.561
264.972	20.2385	-j4.273	16.067	0.088	2.491	5.277	2.390	55.016	1.217	1.543
277.386	20.9605	-j5.834	16.035	0.089	2.424	5.185	2.433	55.044	1.217	1.513
289.800	22.5207	-j9.027	15.959	0.092	2.309	5.012	2.535	55.144	1.217	1.461
302.214	26.1379	-j15.681	15.772	0.097	2.159	4.713	2.788	55.481	1.217	1.378
314.628	29.3309	-j13.379	16.033	0.097	1.880	4.734	2.435	59.532	1.217	1.438
327.041	31.6348	-j10.248	16.248	0.098	1.685	4.781	2.146	63.187	1.217	1.506
339.455	32.5910	-j6.587	16.420	0.099	1.579	4.857	1.910	66.110	1.217	1.587
351.869	32.4426	-j3.150	16.544	0.100	1.551	4.947	1.731	68.134	1.217	1.675
4.283	31.7170	-j0.226	16.630	0.101	1.576	5.040	1.599	69.447	1.217	1.766
16.697	30.6180	+j2.235	16.687	0.102	1.639	5.135	1.504	70.169	1.217	1.861
29.110	29.2494	+j4.308	16.721	0.104	1.729	5.235	1.443	70.375	1.217	1.963
41.524	27.6684	+j6.069	16.736	0.105	1.846	5.343	1.416	70.094	1.217	2.073
53.938	25.8754	+j7.558	16.728	0.106	1.993	5.463	1.430	69.294	1.217	2.186
quency (GH	2):	Impedance-Mat	ching Target	Select		List		List		Zoom k
1.0000 GHz 1.0000 GHz 1.1000 GHz		O Point select	ed nference	Circle	A (Power) B (Contour) C (Efficiency)		mpedance Admittance Reflection	 Actual Intrinsi 	load c load	Zoom Q

The performance on the circumference of a constant power contour is listed here (select the frequency of interest from the list provided). The optimum point selected on the contour is high-lighted and can be changed.

A circle (fundamental frequency targets) can be fitted automatically to each contour or the optimum point on each contour for impedance-matching purposes.

The option to target circles centred on the optimum point of each contours was selected here. The area inside each of these circles will be targeted.



Circle D (Target)

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1.2000 GHz 1.3000 GHz

Reset

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The Performance Associated with the Optimum | Specified Terminations

F (GHz)	MAG[FL]	ANG [FL]	Pmu (dBm)	GT (dB)	VSWRload	VSWRin	Eff (%)	00pt (°)	SSF	LSF
1.0000	0.2670	165.159	39.978	16.721	1.729	5.235	70.375	29.110	1.217	1.963
1.1000	0.2746	164.528	39.978	16.967	1.758	4.048	70.378	31.966	1.299	2.001
1.2000	0.2828	164.007	39.978	17.217	1.789	3.158	70.376	34.883	1.403	2.005
1.3000	0.2909	163.714	39.978	17.420	1.821	2.537	70.365	37.676	1.516	1.974
1.4000	0.2994	163.516	39.978	17.534	1.856	2.173	70.364	40.531	1.593	1.915
1.5000	0.3082	163.470	39.979	17.536	1.892	2.075	70.366	43.386	1.574	1.831
1.6000	0.3170	163.551	39.979	17.430	1.929	2.230	70.362	46.179	1.469	1.728
1.7000	0.3259	163.727	39.979	17.238	1.968	2.588	70.357	49.034	1.343	1.613
1.8000	0.3348	164.032	39.979	16.999	2.007	3.091	70.355	51.828	1.237	1.491
1.9000	0.3435	164.430	39.980	16.752	2.048	3.690	70.353	54.559	1.156	1.370
2.0000	0.3524	164.912	39.980	16.530	2.090	4.332	70.347	57.352	1.097	1.255
2.1000	0.3612	165.472	39.980	16.355	2.132	4.961	70.343	60.083	1.053	1.150
2.2000	0.3701	166.303	39.980	16.225	2.176	5.516	70.317	62.814	1.020	1.059
2.3000	0.3786	167.017	39.981	16.159	2.220	5.952	70.313	65.545	0.994	0.983
2.4000	0.3872	167.783	39.981	16.134	2.264	6.244	70.305	68.276	0.975	0.924
2.5000	0.3953	168.604	39.981	16.128	2.308	6.395	70.301	70.945	0.960	0.882
2.6000	0.4035	169.492	39.982	16.115	2.353	6.445	70.305	73.614	0.950	0.854

Display	Harmonic Control	Transmission Phase Control	
Impedance Intrinsic termination	Save ZLi	NCT-Network	Phase Control Passband Frequency
Reflection	Set Hm_ZL	CT-Network	Center frequency
	Set Hm_ZL (Asym)	PI-Network	Highest frequency
Display <u>G</u> raph Display <u>Impedances</u>		Stepped ML	Lowest gain frequency
	Harmonic Reactance Harmonic Traps	Δθ: 0.0 ° [0, 360]	Phase Control Help
	Ignore Hrm_ZL	Explore Pre-Match	
		< <u>B</u> ack	Next > Cancel Help

The performance at the optimum point on each power contour is listed on this page.

The Set Harmonic ZL and Set Harmonic ZL (Asymmetrical) commands can be used to set impedance-matching targets for the harmonic terminations. Class-B operation will be targeted here.

Note the Harmonic Traps command. Harmonic traps can be added to the matching networks to be synthesized as fixed elements by using this command. The option to export the traps selected directly to the circuit file is also provided.

The Explore Pre-Match option (CMA networks) provides an alternative to the Impedance-Matching module. The transmission phase-shift can be controlled directly by using this option (The CMA networks are derived from PI-networks and T-networks; two cascaded lines are also allowed). The intrinsic load terminations cannot yet be controlled directly by using this option.

The pre-match option will not be used in the presentation.



Optimum Power Terminations



The Display Graph command provided on the wizard page was used to display the circles to be targeted in the Impedance-matching module. The constant power contours and the maximum efficiency lines are also shown.

Note that the origins of the maximum efficiency lines are located in a relatively small area. This area can be targeted by targeting power levels close to the peak levels. A good alternative is to target the line segment defined by the intersects of the maximum efficiency lines with the zero reactance line. This can be done by using a segmented taper transmission line.

Also note the eye formed by the circles targeted here. This area could also be targeted.

Power close to the targeted levels can be obtained at all of the frequencies shown by targeting the red circle at the bottom of the plot. The efficiency will, however, be lower that the level targeted.

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Z02=50.00Ω

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The Performance Associated with the Optimum | Specified Terminations

F (GHz)	RLi (Ω)	XLi (Ω) P	mu (dBm)	GT (dB)	VSWRa	VSWRin	Eff (%)	Tun	SSF	LSF
1.0000	31.942	+j0.138E-3	39.978	16.721	1.443	5.235	70.375	0.104	1.217	1.963
1.1000	31.942	-j0.004	39.978	16.967	1.489	4.048	70.378	0.152	1.299	2.001
1.2000	31.944	+j0.006	39.978	17.217	1.517	3.158	70.376	0.224	1.403	2.005
1.3000	31.941	-j0.006	39.978	17.420	1.527	2.537	70.365	0.254	1.516	1.974
1.4000	31.935	-j0.004	39.978	17.534	1.518	2.173	70.364	0.231	1.593	1.915
1.5000	31.933	+j0.001	39.979	17.536	1.493	2.075	70.366	0.219	1.574	1.831
1.6000	31,930	-j0.005	39.979	17.430	1.458	2.230	70.362	0.236	1.469	1.728
1.7000	31.925	+j0.006	39.979	17.238	1.420	2.588	70.357	0.287	1.343	1.613
1.8000	31.923	+j0.006	39.979	16.999	1.384	3.091	70.355	0.347	1.237	1.491
1.9000	31.919	-j0.005	39.980	16.752	1.354	3.690	70.353	0.312	1.156	1.370
2.0000	31.915	+j0.726E-3	39.980	16.530	1.332	4.332	70.347	0.235	1.097	1.255
2.1000	31.911	-j0.005	39.980	16.355	1.318	4.961	70.343	0.190	1.053	1.150
2.2000	31.817	+j0.040E-3	39.980	16.225	1.314	5.516	70.317	0.173	1.020	1.059
2.3000	31.806	+j0.002	39.981	16.159	1.313	5.952	70.313	0.179	0.994	0.983
2.4000	31.806	+j0.006	39.981	16.134	1.314	6.244	70.305	0.213	0.975	0.924
2.5000	31.801	+j0.081E-3	39.981	16.128	1.317	6.395	70.301	0.308	0.960	0.882
2.6000	31.792	-j0.003	39.982	16.115	1.318	6.445	70.305	0.552	0.950	0.854



The performance at the optimum point on each power contour is listed in the table shown.

The intrinsic load impedance targeted is around 31.9 Ohm. The impedance required at the insertion point for the matching network is around 29 Ohm and lower (see the next slide). Take note of these levels. When the matching networks synthesized do not allow for biasing the transistor, fixed components can be added to the matching network. Any extra shunt elements added should ideally present impedances significantly higher than the impedances targeted (say, at least three to four times higher).

X



The Performance Associated with the Optimum | Specified Terminations

F (GHz)	RL (Ω)	XL (Ω)	Pmu (dBm)	GT (dB)	VSWRa	VSWRin	Eff (%)	Tun	SSF	LSF
1.0000	29.249	+j4.308	39.978	16.721	1.443	5.235	70.375	0.104	1.217	1.963
1.1000	28.807	+j4.565	39.978	16.967	1.489	4.048	70.378	0.152	1.299	2.001
1.2000	28.334	+j4.798	39.978	17.217	1.517	3.158	70.376	0.224	1.403	2.005
1.3000	27.858	+j4.965	39.978	17.420	1.527	2.537	70.365	0.254	1.516	1.974
1.4000	27.355	+j5.106	39.978	17.534	1.518	2.173	70.364	0.231	1.593	1.915
1.5000	26.841	+j5.201	39.979	17.536	1.493	2.075	70.366	0.219	1.574	1.831
1.6000	26.327	+j5.253	39.979	17.430	1.458	2.230	70.362	0.236	1.469	1.728
1.7000	25.805	+j5.273	39.979	17.238	1.420	2.588	70.357	0.287	1.343	1.613
1.8000	25.286	+j5.245	39.979	16.999	1.384	3.091	70.355	0.347	1.237	1.491
1.9000	24.776	+j5.181	39.980	16.752	1.354	3.690	70.353	0.312	1.156	1.370
2.0000	24.263	+j5.083	39.980	16.530	1.332	4.332	70.347	0.235	1.097	1.255
2.1000	23.762	+j4.952	39.980	16.355	1.318	4.961	70.343	0.190	1.053	1.150
2.2000	23.248	+j4.721	39.980	16.225	1.314	5.516	70.317	0.173	1.020	1.059
2.3000	22.767	+j4.522	39.981	16.159	1.313	5.952	70.313	0.179	0.994	0.983
2.4000	22.293	+j4.297	39.981	16.134	1.314	6.244	70.305	0.213	0.975	0.924
2.5000	21.844	+j4.044	39.981	16.128	1.317	6.395	70.301	0.308	0.960	0.882
2.6000	21.399	+j3.762	39.982	16.115	1.318	6.445	70.305	0.552	0.950	0.854

Display	Harmonic Control	Transmission Phase Control	
	Save ZLi	NCT-Network	Characterized Passband Frequency
O Reflection	Set Hrm_ZL	CT-Network	Center frequency
	Set Hm_ZL (Asym)	PI-Network	O Highest frequency
Display <u>G</u> raph Display <u>I</u> mpedances		Stepped ML	 Lowest gain frequency
	Harmonic Reactance	۸ ۵ · 0.0 °	Phase Control Help
	Harmonic Traps	[0, 360]	
	✓ Ignore Hrm_ZL	Explore Pre-Match	
		< Back	Next > Cancel Help

The impedance required at the insertion point for the matching network is around 29 Ohm and lower.

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The Performance Associated with the Optimum | Specified Terminations

1.0000	29.249	+j4.308	39.978	16.721	1.443	Harmonic Control Spee	cifications				
1.1000	28.807	+j4.565	39.978	16.967	1.489						
1.2000	28.334	+j4.798	39.978	17.217	1.517	2nd Harmonic (H2)				Fundamental-Frequer	ncy Terminations
1.3000	27.858	+j4.965	39.978	17.420	1.527	the second second second second		ZF 2ndH:	2.50		
1.4000	27.355	+j5.106	39.978	17.534	1.518	Control 2nd harmo	nic			Use RLi opt	
L.5000	26.841	+j5.201	39.979	17.536	1.493	terminations		RangeScaFac:	1 000	ope	
L.6000	26.327	+j5.253	39.979	17.430	1.458			<1.0>	1.000	RLi opt sc	ale factor:
7000	25.805	+j5.273	39.979	17.238	1.420			1.07	[0.01; 1.0]		
.8000	25.286	+j5.245	39.979	16.999	1.384	 Low second-harmo 	onic impedance	AnumCanau		1.000)
.9000	24.776	+j5.181	39.980	16.752	1.354	$ZLi_2ndH = j ZLi_1$	_Fund / ZF_2ndH	Asymspes:	0.000	[0.7E)	1 75]
.0000	24.263	+j5.083	39.980	16.530	1.332	O High second-harmo	onic impedance	<u></u>	C:1L:-1LIC:0	[0.75;	1.75]
2.1000	23.762	+j4.952	39.980	16.355	1.318	ZLi 2ndH = j ZLi	Fund x ZF 2ndH	Minimum			
2.2000	23.248	+j4.721	39.980	16.225	1.314		-		5.00	Use saved 71	
.3000	22.767	+j4.522	39.981	16.159	1.313			in un sic Q.		USE Saved ZLI	
2.4000	22.293	+j4.297	39.981	16.134	1.314	Width of the H2	0.10000 GHz			ZLi scale fa	actor:
.5000	21.844	+j4.044	39.981	16.128	1.317	transition band:					
.6000	21.399	+j3.762	39.982	16.115	1.318					1.000	
						3rd Harmonic (H3)				[0.75.	1 75]
play				Harmonic Control		Carbol Dallaren	-1-	ZF_3rdH:		[0.75;	1./5]
				0		Control 3rd narmor	nic		2.50		
Impedance	e 🗌 let	incic terminativ		Save ZU		terminations		RangeScaFac:		Clipping Contour Opti	00
Reflection		In Sic termination	011					<1.0>	1.000	cipping contour opuc	511
				Set Hrm_ZL		High third-harmoni	ic impedance		[0.01:1.0]	Use H2 dipping cor	ntours
				0.111 71 /4		ZLi 3rdH = i ZLi	Fund x ZF 3rdH	AsymSpes:	[0.01, 1.0]		
				Set Hm_ZL (As	/m)	O law third barmonia	s impedance	<0>	0.000	Reduce the assum	ed dc voltage by
Display Gra	aph	Display Impeda	ances			U Low third-harmonic	c impedance			using the bounda	ary line intercept
						2LI_3rdH =) 2LI_	Fund / ZF_3rdH	Minimum	C:1L:-1L C:0		
								intrinsic Q:	5.00	Correction voltage	0.500 <0.5>
				Harmonic Reacta	ance	Width of the H3	0.10000 GHz			scale factor:	
				Harmonic Tran	10	transition band:	Griz				[0; 0.95]
				riamonic may							
				Ignore Hrm Z		0					
						OK	Cancel	H	lelp	Reset Clas	iS
						Rack	Next	Cancel	Help		
						(Dack	Tieve	Carloci	Ticip		

The Set Harmonic Z_L command was selected.

Low or high impedance second or third harmonic intrinsic terminations can be targeted. Because Class-B operation is required, low harmonic impedances will be targeted (low relative to the fundamental-frequency impedances).



The second and third harmonic bands in this example overlap the passband. The third harmonic band also overlaps the second harmonic band. The fundamental targets override the harmonic targets in the ADW, while the second harmonic targets generally override the third harmonic targets.

Transition bands can be defined for the second harmonics and the third harmonics. 0.4 GHz will be used for the second harmonic and 0.1 GHz will be used for the third. Because shorts are required for both harmonic bands, the transition band for the third harmonic could be set to zero.



The Performance Associated with the Optimum | Specified Terminations **Optimum Power Terminations** F (GHz) RL (Ω) XL (Ω) Pmu (dBm) GT (dB) VSWRa 1.0000 1.443 29.249 +j4.308 39.978 16.721 39.978 16.967 1.489 1.1000 28.807 +j4.565 39.978 17.217 1.517 1.2000 28.334 +j4.798 1.3000 27.858 +j4.965 39.978 17.420 1.527 39.978 17.534 1.518 1.4000 27.355 +j5.106 39.979 17.536 1.493 1.5000 26.841 +j5.201 +j5.253 39.979 17.430 1.458 1.6000 26.327 17.238 1.7000 25.805 +j5.273 39.979 1.420 1.8000 25.286 +j5.245 39.979 16,999 1.384 16.752 1.354 1.9000 24.776 +j5.181 39.980 +j5.083 39.980 16.530 1.332 2.0000 24.263 2,1000 23.762 +j4.952 39.980 16.355 1.318 +j4.721 39.980 16.225 1.314 2.2000 23.248 2.3000 22.767 +j4.522 39.981 16.159 1.313 39.981 16.134 1.314 2.4000 22.293 +j4.297 2.5000 21.844 +j4.044 39.981 16.128 1.317 39.982 16.115 1.318 2.6000 21.399 +j3.762 Harmonic Control Display Save ZLi Impedance Intrinsic termination Reflection Set Hrm_ZL Set Hrm_ZL (Asym) Display Graph Display Impedances Harmonic Reactance Intrinsic Harmonic Angles Targeted Harmonic Traps 2ndH: [180.0°,180.0°]; Δ=28.7° Z0=50.00 Zoom 3rdH: [180.0°,180.0°]; ∆=28.7° Z0=50.00 Ignore Hrm_ZL



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The fundamental-frequency and harmonic targets at the insertion point for the matching network.

Options are provided to hide the third or the second harmonic targets.

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Cancel

Help

< Back

<u>N</u>ext >



Optimum Power Terminations



Hide Trace Hide Trace Hide s21w Hide 2nd harmonic traces Hide 3rd harmonic traces Hide harmonic markers Hide reactance range traces Show Harmonic Markers At **All Frequencies** O Specified Frequency GHz \sim Save Contours Delete Saved Contours Z02=50.00Ω

X

The targets can be displayed for all the passband frequencies or for a specific passband frequency. The associated intrinsic impedances will be near shorts for terminations at the centre of the range of external reflection coefficients shown for each harmonic.

Harmonic sectors are fitted automatically to the areas defined by the harmonic markers. A sector is defined by a local origin and two intersects with the Smith chart edge.

Harmonic sectors will also be fitted to the intrinsic targets if the relevant option was selected.



Optimum Power Terminations



The second and third harmonic targets associated with 3.9 GHz.

Note that the harmonic areas to be targeted rotate anti-clockwise with frequency. It will not be possible to obtain near shorts for all the harmonics with the passband targeted here.

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GHz

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Harmonic Termination	s Required

Ffund (GHz)	XB_2ndH	XE_2ndH	XB_3rdH	XE_3rdH
1.0000	-31.717	-0.387	-48.367	-6.728
1.1000	-34.418	-1.636	-55.621	-8.714
1.2000	-37.377	-2.891	-64.655	-10.768
1.3000	-40.643	-4.154	-76.389	-12.911
1.4000	-44.277	-5.434	-92.242	-15.162
1.5000	-48.352	-6.730	-115.269	-17.546
1.6000	-53.020	-8.047	-152.095	-20.096
1.7000	-58.364	-9.394	-220.744	-22.849
1.8000	-64.599	-10.774	-397.504	-25.850
1.9000	-72.008	-12.191	-1.935E3	-29.156
2.0000	-80.969	-13.654	673.029	-32.846
2.1000	-92.114	-15,169	285.427	-37.018
2.2000	-105.710	-16.767	182.323	-41.846
2.3000	-124.279	-18.413	131.914	-47.440
2.4000	-150.320	-20.133	102.421	-54.095
2.5000	-189.165	-21.944	83.037	-62.204

List	ОК
 Reflection coefficients (Z0=50) Reflection coefficients (Z0sc) 	Cancel
Reactance values	Help

The reactance ranges to be targeted for the second and third harmonics are listed here. Note the anticlockwise rotation of the targets with increasing frequency.

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Second and Third Harmonic Traps

Second-Harmonic Traps	Third-Harmonic Traps				
L H2_L (OS) (wcFuQL:4.26 wcFuQs:1.27): SST Null at F_H2L= 4.40000GHz. ML: 20=43.75Ω Ang=127.723° @ 3.90000GHz. XfuL:-174.3Ω XfuC:-56.3Ω XfuH:-11.7Ω Fnull_cSST:15.59055GHz; wcFuX:-14.3Ω.	L H3_L (IS) (wcFuQs:0.37 wcFuQL:0.73); SST Null at F_H3L= 8.10000GHz. ML: 20=43.75Ω Ang=48.072° @ 3.90000GHz. XfuL:-331.0Ω XfuC:-129.4Ω XfuH:-68.9Ω Fnull_cSST:8.10000GHz; wcFuX:28.9Ω.				
C H2 Gap Center (OS) (wcFuQL:1.26 wcFuQs:0.43): SST Null at F_H2C= 6.00000GHz. ML: 20=43.75Ω Ang=82.457° @ 3.90000GHz. XfuL:-242.6Ω XfuC:-89.5Ω XfuH:-39.8Ω Fnull_cSST:6.99029GHz; wcFuX:-35.8Ω.	C H3 Gap Center (IS) (wcFuQs:0.34 wcFuQL:0.55): SST Null at F_H3C= 9.90000GHz. ML: 20=43.75Ω Ang=29.862° @ 3.90000GHz. XfuL:-406.2Ω XfuC:-162.4Ω XfuH:-91.3Ω Fnull_cSST:9.90000GHz; wcFuX:22.5Ω.				
H H2_H: SST Null at F_H2H= 7.80000GHz. ML: 20=43.75Ω Ang=60.562° @ 3.90000GHz. XfuL:-318.4Ω XfuC:-123.8Ω XfuH:-65.0Ω Fnull_cSST:7.80000GHz; wcFuX:30.3Ω.	H H3_H (IS) (wcFuQs:0.32 wcFuQL:0.44): SST Null at F_H3H= 11.70000GHz. ML: 20=43.75Ω Ang=18.285° @ 3.90000GHz. XfuL:-481.2Ω XfuC:-194.7Ω XfuH:-112.6Ω Fnull_cSST:11.70000GHz; wcFuX:18.6Ω.				
P H2_P Trap (OS) (wcFuQL:1.17 wcFuQs:0.54): SST_Null: H2C=6.00000GHz; OST_Null: F=7.79221GHz. ML: 20=43.75Ω Ang=82.457° @ 3.90000GHz. XfuL:42.5Ω XfuC:-324.1Ω XfuH:-73.4Ω	P H3_P Trap (IS) (wcFuQs:0.87 wcFuQL:1.73): OST_Null: H3L=8.10000GHz; SST_Null: F=8.10000GHz. ML: Z0=43.75Ω Ang=48.072° @ 3.90000GHz. XfuL:28.9Ω XfuC:268.3Ω XfuH:-73.4Ω				
Second-Harmonic and Third-Harmonic Trap	Characteristic Impedances				
M H2_H and H3_L (OS) (Err:56.5°; wcFuQL:1.73 wcFuQs:0.87):	Double Traps				
Nulls at F2=7.80000GHz and F3=8.10000GHz. ML: Z0=43.75Ω Ang=60.562° @ 3.90000GHz. XfuL:29.0Ω XfuG:104.9Ω XfuC:295.9Ω XfuH:-69.0Ω	ZOML_min: 7.50 ZOML_max: 80.0	00			
Single Trap Connecting Line	Z0ML single 43.75 Z0OST: 65.0	00			
Matching network 0.00 ° at 3.90000GHz	ZOSST: 65.00 ZOOST stepped line: 65.0	0			
Double Trap Options	(ML: Main line: OST: Open-ended stub: SST: Shorted stu	њ.)			
Matching network connecting 20.00 ° at 3.90000GHz					
Allow OST stepped line	Target the optimum reactance with each trap wcQs_NoTrap Export selected traps to the circuit file wcQL_NoTrap	os: 0.2 os: 0.0			
Matching Network Side Allocation					
Maximum ML length for an input	Re-Calculate OK Cancel	Help			
5U.UU 9 st 3 00000CH*					

- 5):

- 10000GHz.

Help

Harmonic traps can be used to provide the required intrinsic impedance at specific frequencies. Potential traps are listed here for a number of second and third harmonic frequencies. When an SST option is set, the trap will be created with a shorted stub. The default is to use an open-ended stub.

When the series transmission line (ML) associated with a trap is short, the trap can be added to the circuit before a matching network is designed. Traps with longer main lines can be added on the output side of the matching network, but it is unlikely that the desired transmission phase shift required for an intrinsic short will be obtained with the matching network in place. The harmonic will, however, be filtered from the output.

Note that the traps marked with a P consist of a shorted stub in parallel with an openended stub.

Ideally a trap should not load the circuit significantly at the fundamental frequencies. The loading imposed is measured by calculating the worst-case fundamental-frequency source and load Qs, as well as the shunt reactance presented by the trap at a number of passband frequencies. The worst-case Qs of the terminations (no loading) are listed in the lower RHS corner of the table.

The trap with the shortest main-line length (18.285 degrees at 3.9GHz) is the 11.7 GHz trap. The loading associated with this trap will be minimal. Note that the H2 P trap may be a good option for feeding in the drain bias. The shunt impedance presented is higher than 42.5 Ohm inside the passband (still significant).

Up to two traps can be selected from the table. The selected traps can be exported directly to the circuit file or can be added as fixed components to the matching networks to be synthesized.

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Second and Third Harmonic Traps

Second-Harmonic Traps	Third-Harmonic Traps
L H2_L (OS) (wcFuQL:2.06 wcFuQs:0.51): ✓ SST Null at F_H2L = 4.40000GHz. ML: 20=43.75Ω Ang=127.723° @ 3.90000GHz. XfuL:56.3Ω XfuC:-452.1Ω XfuH:-24.2Ω	L H3_L (IS) (wcFuQs:0.95 wcFuQL:1.88): SST Null at F_H3L=8.10000GHz. ML: Z0=43.75Ω Ang=48.072° @ 3.90000GHz. XfuL:26.6Ω XfuC:87.3Ω XfuH:1116.0Ω Fnull_cOST:8.10000GHz; wcFuX:28.9Ω.
□ c H2 Gap Center (OS) (wcFuQL:1.33 wcFuQs:0.63): ✓ SST Null at F_H2C= 6.00000GHz. ML: 20=43.75Ω Ang=82.457° @ 3.90000GHz. XfuL:37.5Ω XfuC:200.0Ω XfuH:-127.6Ω Fnull_cOST:7.79221GHz; wcFuX:42.5Ω.	C H3 Gap Center (IS) (wcFuQs:1.22 wcFuQL:2.34): SST Null at F_H3C= 9.90000GHz. ML: 20=43.75Ω Ang=29.862° @ 3.90000GHz. XfuL:21.3Ω XfuC:62.0Ω XfuH:187.8Ω Fnull_cOST:9.90000GHz; wcFuX:22.5Ω.
H H2_H: ✓ SST Null at F_H2H= 7.80000GHz. ML: Z0=43.75Ω Ang=60.562° @ 3.90000GHz. XfuL:27.7Ω XfuC:94.2Ω XfuH:-100000000.0Ω Fnull_cOST:7.80000GHz; wcFuX:30.3Ω.	H H3_H (IS) (wcFuQs:1.49 wcFuQL:2.80): Null at F_H3H= 11.70000GHz. ML: 20=43.75Ω Ang=18.285° @ 3.90000GHz. XfuL: 17.9 XfuC:48.8 XfuH:112.6 Fnull_cOST:11.70000GHz; wcFuX:18.6Ω.
P H2_P Trap (OS) (wcFuQL:1.17 wcFuQs:0.54): SST_Null: H2C=6.00000GHz; OST_Null: F=7.79221GHz. ML: Z0=43.75Ω Ang=82.457° @ 3.90000GHz. XfuL:42.5Ω XfuC:-324.1Ω XfuH:-73.4Ω	P H3_P Trap (IS) (wcFuQs:0.87 wcFuQL:1.73): OST_Null: H3L=8.10000GHz; SST_Null: F=8.10000GHz. ML: Z0=43.75Ω Ang=48.072° @ 3.90000GHz. XfuL:28.9Ω XfuC:268.3Ω XfuH:-73.4Ω
Second-Harmonic and Third-Harmonic Trap	Characteristic Impedances
M H2_H and H3_L (OS) (Err:56.5°; wcFuQL:1.66 wcFuQs:0.82):	Double Traps
Nulls at F2=7.80000GHz and F3=8.10000GHz. ML: Z0=43.75Ω Ang=60.562° @ 3.90000GHz. Xfu: 29.00 Xfu: 104.90 Xfu: 295.90 Xfu: 69.00	Z0ML_min: 7.50 Z0ML_max: 80.00
Single Trap Connecting Line	Z0ML single 43.75 Z0OST: 65.00
Matching patwork	trap: Z0OST
connecting line length: 0.00 ° at 3.90000GHz	ZOSST: 65.00 stepped line: 65.00
Double Trap Options	(ML: Main line: OST: Open-ended study: SST: Shorted study)
Matching network connecting 20.00 ° at 3,90000GHz	
line length [5;60]:	Target the optimum reactance with each trap wcQs_NoTraps: 0.2
	Export selected traps to the circuit file wcQL_NoTraps: 0.00
Allow OST stepped line	
Allow OST stepped line Matching Network Side Allocation	
Allow OST stepped line Matching Network Side Allocation Maximum ML length for an input old (S) trace 100.1201 c60801 60.00 orat 3.90000GHz	Re-Calculate OK Cancel Help

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The SST options were set here to view the loading associated with shorted stub traps. The loading of the 6.0 GHz second harmonic trap is above 37.5 Ohm in the passband, but this is not high enough to not have a degrading effect on the performance.



The Performance Associated with the Optimum | Specified Terminations

F (GHz)	RL (Ω)	XL (Ω)	Pmu (dBm)	GT (dB)	VSWRa	VSWRin	Eff (%)	Tun	SSF	LSF
1.0000	29.249	+j4.308	39.978	16.721	1.443	5.235	70.375	0.104	1.217	1.963
1.1000	28.807	+j4.565	39.978	16.967	1.489	4.048	70.378	0.152	1.299	2.001
1.2000	28.334	+j4.798	39.978	17.217	1.517	3.158	70.376	0.224	1.403	2.005
1.3000	27.858	+j4.965	39.978	17.420	1.527	2.537	70.365	0.254	1.516	1.974
1.4000	27.355	+j5.106	39.978	17.534	1.518	2.173	70.364	0.231	1.593	1.915
1.5000	26.841	+j5.201	39.979	17.536	1.493	2.075	70.366	0.219	1.574	1.831
1.6000	26.327	+j5.253	39.979	17.430	1.458	2.230	70.362	0.236	1.469	1.728
1.7000	25.805	+j5.273	39.979	17.238	1.420	2.588	70.357	0.287	1.343	1.613
1.8000	25.286	+j5.245	39.979	16.999	1.384	3.091	70.355	0.347	1.237	1.491
1.9000	24.776	+j5.181	39.980	16.752	1.354	3.690	70.353	0.312	1.156	1.370
2.0000	24.263	+j5.083	39.980	16.530	1.332	4.332	70.347	0.235	1.097	1.255
2.1000	23.762	+j4.952	39,980	16.355	1.318	4.961	70.343	0.190	1.053	1.150
2.2000	23.248	+j4.721	39.980	16.225	1.314	5.516	70.317	0.173	1.020	1.059
2.3000	22.767	+j4.522	39.981	16.159	1.313	5.952	70.313	0.179	0.994	0.983
2.4000	22.293	+j4.297	39.981	16.134	1.314	6.244	70.305	0.213	0.975	0.924
2.5000	21.844	+j4.044	39.981	16.128	1.317	6.395	70.301	0.308	0.960	0.882
2.6000	21.399	+j3.762	39.982	16.115	1.318	6.445	70.305	0.552	0.950	0.854

Display	Harmonic Control	Transmission Phase Control	
Impedance Reflection	Save ZLi	NCT-Network	Phase Control Passband Frequency
	Set Hm_ZL Set Hm_ZL (Asym)	PI-Network	Center frequency Highest frequency
Intrinsic Harmonic Angles Targeted	Harmonic Reactance	Stepped ML	Phase Control Help
2ndH: [180.0°,180.0°]; Δ=28.7° Z0=50.00 3rdH: [180.0°,180.0°]; Δ=28.7° Z0=50.00	Harmonic Traps	[0, 360]	
		< <u>B</u> ack	Next > Cancel Help

The Next command has been selected to proceed to solving the defined matching problem.

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Power Matching	Wizard -	Data File	Name	and Title
----------------	----------	-----------	------	-----------

The specifications of the matching problem to be solved will be stored in a data file. The root part of the data file name and the title to be used in the file can be specified here. Note that the file type should not be specified and a file path is also not allowed.

Impedance-Matching Data File

Data file name (Type: .mmi):

ADWDSGN4SYN1

<u>T</u>itle:

Power matching

Default Synthesis Option

Synthesize

Lumped or non-commensurate distributed solutions
 Commensurate distributed solutions

The default name for the matching network file is shown here. The option to solve the matching problem with non-commensurate networks was selected.

Cancel

Help

< Back

Next >

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CIL/CIR Impedance-Matching Wizard

You have successfully completed the steps of the CIL or CIR wizard. If the CMA command was used, or traps were selected for export, the associated schematic elements will be inserted into the circuit file next. If neither of these options were not chosen, the Impedance-Matching wizard will be launched next to solve the matching problem defined.

It is recommended that you save the circuit file after closing this wizard.

Save the circuit file automatically

C:\Users\USER\Documents\Ampsa\AmpsaADW23H\Examples\Power Amplifiers\Cree10

Launch the Impedance-Matching Module

The matching problem has been defined by the CIL wizard. The next step is to solve the problem.

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Cancel

Help

< <u>B</u>ack

Finish

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The Matching wizard was launched and impedance-matching networks can now be synthesized.

Solutions to the matching problem will be synthesized next.





It is generally a good approach to try lumped solutions to a matching problem first (Use the Network Type ribbon command). Insight into the problem can be gained by doing this before proceeding to distributed solutions.

A lumped solution to the matching problem is shown here. The drain bias can be fed in through the inductor if the *dc* short is replaced with an RF short.





The topology constraints used when the lumped solution shown was synthesized.

Note the bias-type option. Options are provided to synthesize networks allowing biasing on the input and/or output sides of the matching networks.





The effect of reducing the second harmonic transition band to 0.3 GHz is shown here.

A conical coil or a solenoidal coil can be used to feed in the drain bias.





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ADWDSGN4SYN1.mmi - MN Terminations (SC) 🗙

							Second-Harmo	nic Terminat	ions					
(GHz)	MAG[Ss]	ANG[Ss]	MAG[SL]	ANG[SL]	GT (dB)									
0000	0 2763	194 84	0 69008-3	270 04	> -0 1609	Cancel	F (GHz)	MAG[For]	ANG[For]	FangB (°)	<pre>FangE (°)</pre>	RL (Ω)	XL (Ω)	
.1000	0.2842	195.47	0.7600E-3	270.04	> -0.1613	Help	2,0000	0.7708	204.75	244.78	180.89	49,990	-0.140	Cancel
.2000	0.2926	195.99	0.8361E-3	263.18	> -0.1620		2.2000	0.7681	207.37	249.09	183.76	49.980	-0.150	
.3000	0.3009	196.29	0.9056E-3	263.71	> -0.1625		2.4000	0.9439	230.08	253.56	186.62	49,980	-0.170	Help
.4000	0.3098	196.48	0.9752E-3	264.17	> -0.1631	Insert Row	2.6000	0.9412	233.50	258.21	189.49	49.980	-0.180	
.5000	0.3188	196.53	0.0010	264.57	> -0.1636		2.8000	0.9384	237.02	263.06	192.40	49.970	-0.190	
.6000	0.3279	196.45	0.0011	264.92	> -0.1643	Delete Row	3.0000	0.9356	240.65	268.08	195.33	49.970	-0.210	Interpolate
.7000	0.3371	196.27	0.0012	265.18	> -0.1650		3.2000	0.9323	244.39	273.36	198.29	49.970	-0.220	
.8000	0.3462	195.97	0.0012	265.46	> -0.1657	Paste Deleted	3.4000	0.9290	248.25	278.82	201.27	49.960	-0.230	
9000	0.3553	195.57	0.0013	265.71	> -0.1664		3.6000	0.9254	252.23	284.52	204.31	49.960	-0.240	
.0000	0.3644	195.09	0.0014	265.93	> -0.1672	Internolate	3.8000	0.9217	256.35	290.45	207.40	49.950	-0.260	
.1000	0.3734	194.53	0.0015	266.14	> -0.1680	inter <u>p</u> olate	4.0000	0.9179	260.62	296.61	210.54	49.950	-0.270	
.2000	0.3824	193.70	0.0015	262.54	> -0.1663		4.2000	0.9138	265.03	303.01	213.76	49.940	-0.280	
.3000	0.3912	192.98	0.0016	262.88	> -0.1670	Convert Circles	4.4000	0.9100	269.51	309.37	217.08	49.940	-0.300	
.4000	0.4000	192.22	0.0017	263.18	> -0.1679		4.6000	0.9057	274.22	316.17	220.43	49.930	-0.310	
.5000	0.4083	191.40	0.0017	263.47	> -0.1687		4.8000	0.9013	279.10	323.20	223.86	49.930	-0.320	
.6000	0.4167	190.51	0.0018	263.69	> -0.1695	Slope Gain	E 0000	0 0070	204 14	200 20	222.20	10 000	-0.000	
.7000	0.4250	189.55	0.0019	263.94	> -0.1704		Second Harmo	nic Targete a	nd Roundaries	Harmonic	Terminatione	Activat	a Specifications At	
.8000	0.4328	188.61	0.0019	261.23	> -0.1713	Sat Fixed Elemente	Second-Harmo	inic targets a	ind boundaries	Harmonic	, reminations	Activat	e opecnications At	
.9000	0.4404	187.60	0.0020	261.54	> -0.1721	Set Tixed Liements	Use angles	s (Z0 =	= 50.00)	Specifie	d for matching		frequencies	Width of H2
.0000	0.4480	186.54	0.0021	261.79	> -0.1730	Demous Fixed Flaments		ance veluee		networ	к	0.		transition ban
						Remove Fixed Elements	Usereacte	ince values			leaved and a		west frequency	
Format		npedance Fit Or	otion				Target pure	elv reactive te	erminations		input side	⊖ Ce	enter frequency	0.30000 G
						Harmonic Control	(Casait	(Faciaia)		0	Output side	Hig	ghest frequency	
		Fit Impedance	e			2nd Harmonic Targets	(Specin	y rongin)				Oot	her frequencies	Error Function
mpedances	s					2nd harmonic largets	- Overlapping Ha	armonic Band	Is Option			0.00		Weight Factor
Admittance	s	Weight				Contraction Tracest	e tenapping m	anno bana	e epiteri	_				
_		Factor: 0.2	<0.0>			3rd Harmonic Targets	Second	harmonic ove	rrides third	🗌 Ignore	H2 terminations			0.1000
Reflection							_							
		[0	1.0; 1.0]			Use worst case error			-	_				

Use the Edit Terminations ribbon command and then select the 2nd Harmonic Targets command to change the transition band for the second harmonics.

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Ready





Distributed networks will be synthesized next.

The Distributed Networks Wizard is used to change the specifications for distributed networks. Use the ribbon command shown to launch the wizard. Any results views must be closed before the wizard can be launched.



Parasitic Components The option to use shunt parallel-plate capacitors instead of open-ended stubs or shunt capacitors is provided here. The parasitic inductance or resonant frequency of any regular capacitors or the parasitic capacitance or resonant frequency to be used for any inductor in the matching network can also be specified here. The option to use shunt capacitors as harmonic traps is also provided. Parasitics Capacitor Inductance or Resonant Frequency Inductance Capacitance or Resonant Frequency Specify inductance (nH) Specify component resonant frequency (Fr_GHz) Specify capacitance (pF) O Specify trap resonant frequency (FTr_GHz) too Specify resonant frequency (GHz) LnH FTr_GHz: 0.000 ٥F 0.000 GHz nH No parasitics for series capacitors Parallel-Plate Capacitors Use shunt parallel-plate capacitors Via hole inductance: 0 nH Pad width (um) Pad length (L; um) 500.00 1.00E3 Pad Z0 (Ohm) Pad length (°) 50.00 0.00 F = 3.900GHz < Back Next > Cancel Help

Distributed/Microstrip Networks Wizard - Capacitor and Inductor Options

Parasitic inductance and capacitance can be specified for capacitors and inductors on this page.

The parasitic inductance or the resonant frequency for the capacitors can be specified. The option to use the shunt capacitors as harmonic traps is also provided.

Ideal lumped components will be used in this presentation.

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Distributed/Microstrip Networks Wizard - Double Stub Options

Minimum electrical lengt	n (°) at which an open-ended	stub 5
should be converted	to a double stub:	
0.00		
pped main-line sections		
Transform double stu	bs to <u>s</u> tepped main-line secti	ons
Maximum <u>w</u> idth (um)	Minimum width (um)	<u>L</u> ength (um)
0.00	0.00	0.00
Lowest Z0 (Ohm)	Highest Z0 (Ohm)	Electrical length (°)
25.00	65.00	30.00
		F = 3.900GHz
Note: Not using resor when open-ended stu	nating sections is usually a go ubs are replaced with stepper t main-line sections)	ood option d main-line

When it is possible, open-ended stubs in an ADW matching network can be transformed automatically to equivalent mainline sections.

A minimum electrical length can be set for the transformation.

The phase responses of the networks synthesized are generally better behaved when this is done.

Help

Distributed/Microstrip Networks Wizard - Z0's

The characteristic impedance of the lines to be used are listed here. The line lengths will be used as variables. The minimum and maximum length to be used for the main line sections are listed too. The minimum length specification is important when stubs can overlap. When distributed networks are required, the characteristic impedances and line lengths should be modified on this page, if necessary. If the associated dimensions were specified previously for microstrip networks, the values listed should be inspected to ensure that the specifications made are realistic.

Main-line Sections Input side Z0: 35.00 Ohm Minimum length: 15.00 ° FpsbH = 3.900GHz	Output side <u>Z</u> 0: <u>35.00</u> Ohm M <u>a</u> ximum length: <u>175.30</u> ° <u>T</u> aper Check	Stub Parameters <u>S</u> ST Z0: 65.00 Ohm SST maximum electrical length: 65.00 ° <u>O</u> ST Z0 (SST Z0Min): <u>35.00</u> Ohm OST maximum electrical length: 65.00 °	Harmonic Traps SST ResFrq (GHz): 11.00 OST ResFrq (GHz): 11.00 OST CNL length (°) at FpsbH [2°; 25°]: 6.0000 Z0OST Minimum: 10.00 Z0OST Maximum: 65.00
Main-line Z0 Search	ML Z0 minimum: 35.00 Ohm Z0 results	ML Z0 maximum: ML Z 45.00 Ohm	Z0 step: 5.00 Ohm
	(< <u>B</u> ack <u>N</u> ext >	Cancel He

When the characteristic impedance specified for a stub allows it, the stub can be designed to provide a transmission null at a specified frequency in addition to providing the fundamental-frequency reactance required.

Different null frequencies can be set for the shorted stubs and the open-ended stubs.

If the option to transform the open-ended stubs to main-line sections was selected, the open-ended stubs will not be used to trap the harmonics.

Some experimentation with the trap frequencies is usually required. Start by setting the resonant frequencies to frequencies in the transition bands.

In this example, the transmission null frequencies were set to 11.0 GHz.

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The second solution obtained with the specifications shown.

Note that the absolute values of the transformation-Q associated with this solution is small (less than 0.68). Better solutions may be obtained by scaling the range of the systematic search done down.





The range of the search was scaled down and the number of potential solutions to be used in secondary searches was increased.

The Transformation Qs ribbon command was used to open the dialog box shown.

To keep the run-time similar, the *Q* increment should be scaled by the same factor as the boundaries.





The fourth solution obtained with the tighter systematic search.

The Export Selected Solution | Existing ADW Circuit File option was used to export this solution to the original circuit file.





Note that new circuits can be created for any of the solutions shown. The exported matching network can then be modified or tuned or optimized before it is used in the original circuit.



The performance obtained in the original circuit with the solution shown.

Ampsa





To allow for biasing the transistor, the schematic editing command shown will be used to convert the *dc* ground associated with the selected inductor to an *ac* ground.



The lumped-element parasitics were ignored when this matching network was synthesized. Parasitic elements can be added to a capacitor by using the command shown after selecting the capacitor. The capacitor value can then be tuned to compensate for the inductance added.

The performance of the matching network could also be improved by tuning or optimization. To tune the network, mark all the elements in the network for optimization first.



The command used to mark a variable for optimization is shown here. Note the Set Bounds command too.

If marked for optimization, the selected variable can be tuned after selecting the Analysis | Summary Table ribbon command.

The circuit must be analysed before the element values can be tuned.



Use the Set Results Views command to set the views to be opened when an element value is tuned. The views can be arranged as required after using the Analyse command. The Summary Table command is used to tune the selected element value.